# **Regulations Compliance Report**



Approved Document L1A, 2013 Edition, England assessed by Stroma FSAP 2012 program, Version: 1.0.4.16 *Printed on 25 March 2019 at 14:47:27* 

| Project Information    | on:  |  |   |                    |
|------------------------|--|--|---|--------------------|
| Assessed By:           | Aymon Winter (ST                           | RO014511)  | Building Type: Flat                             |                    |
| Dwelling Details:      |  |  |   |                    |
| NEW DWELLING           | DESIGN STAGE                               |  | Total Floor Area: 61.7m <sup>2</sup>            |                    |
| Site Reference :       | 49-51 Beulah Hill                          |  |   | 9-73120 A-1-05 PL1 |
| Address :              | A-1-05, 49-51 Beu                          | lah Hill   | Sada Unit Ref: A1-A11                           |                    |
| Client Details:        |  |  |   |                    |
| Name:<br>Address :     | Sada Architecture                          |  |   |                    |
| •                      | s items included w<br>te report of regulat | ithin the SAP calculations.<br>ions compliance.                          |   |                    |
| 1a TER and DER         | R  |  |   |                    |
|                        | ing system: Mains ga                       | as   |   |                    |
| Fuel factor: 1.00 (r   | mains gas)<br>oxide Emission Rate          |  | 17.89 kg/m²                                     |                    |
| •                      | Dioxide Emission Rat                       |  | 12.95 kg/m²                                     | ОК                 |
| 1b TFEE and DF         |  |  | Ŭ   |                    |
| •                      | rgy Efficiency (TFEE                       |  | 44.1 kWh/m²                                     |                    |
| Dwelling Fabric Er     | nergy Efficiency (DFE                      | E)   | 46.4 kWh/m²                                     | <b>F</b> -1        |
| Excess energy = 2      | 2.27 kg/m² (05.1 %)                        |  |   | Fail               |
| 2 Fabric U-value       | ,  |  |   |                    |
| Element                |  | Average  | Highest   |                    |
| External               | wall                                       | 0.16 (max. 0.30)   | 0.23 (max. 0.70)                                | ОК                 |
| Party wal              | I  | 0.00 (max. 0.20)   | -   | ОК                 |
| Floor                  |  | (no floor)   |   |                    |
| Roof<br>Openings       |  | (no roof)<br>1.40 (max. 2.00)  | 1.40 (max. 3.30)                                | ОК                 |
| 2a Thermal bridg       |  | 1.40 (max. 2.00)   | 1.40 (max. 5.50)                                | OK                 |
|                        |  | om linear thermal transmittar  | uces for each junction                          |                    |
| 3 Air permeabilit      |  |  |   |                    |
| Air permeat<br>Maximum | oility at 50 pascals                       |  | 5.00 (design value)<br>10.0                     | ОК                 |
| 4 Heating efficie      | ency                                       |  |   |                    |
| Main Heatir            | ng system:                                 | Database: (rev 440, produc   | ct index 017558):                               |                    |
|                        |  | Brand name: Worcester<br>Model: Greenstar<br>Model qualifier: 34CDi Clas | rs or underfloor heating - mains ga<br>ssic ErP | S                  |
|                        |  | (Combi)<br>Efficiency 89.1 % SEDBUK                                      | 2009  |                    |
|                        |  | Minimum 88.0 %   |   | ОК                 |



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| Secondary heating syst   | em: None  |   |       |
|--|---|---|-------|
| 5 Cylinder insulation  |   |   |       |
| Hot water Storage:   | No cylinder   |   |       |
| 6 Controls   |   |   |       |
| Space heating controls<br>Hot water controls:  | Programmer, room ther<br>No cylinder<br>No cylinder | mostat and TRVs   | ОК    |
| Boiler interlock:  | Yes   |   | ОК    |
| 7 Low energy lights  |   |   |       |
| Minimum  | ts with low-energy fittings                         | 100.0%<br>75.0%   | ОК    |
| 8 Mechanical ventilation   |   |   |       |
| Continuous extract syst<br>Specific fan power:   | em  | 0.15  |       |
| Maximum  |   | 0.7   | OK    |
| 9 Summertime temperature   |   |   |       |
| Overheating risk (Tham<br>Based on:  | es valley):   | Medium  | OK    |
| Overshading:<br>Windows facing: South<br>Windows facing: South<br>Windows facing: North<br>Ventilation rate:<br>Blinds/curtains: | West  | Average or unknown<br>8.1m²<br>6.41m²<br>6.1m²<br>4.00<br>Closed 100% of daylight h | nours |
| 10 Key features  |   | 0.40 \\\\\-214  |       |
| External Walls U-value<br>Party Walls U-value<br>Photovoltaic array  |   | 0.13 W/m²K<br>0 W/m²K   |       |



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| Assessor and House Details          |   |                  |            |  |  |  |
|-------------------------------------|---|------------------|------------|--|--|--|
| Assessor Name:<br>Property Address: | Aymon Winter<br>A-1-05<br>49-51 Beulah Hill | Assessor Number: | STRO014511 |  |  |  |
| Buiding regulation assessment       |   |                  |            |  |  |  |

|   | kg/m²/year |
|---|------------|
| TER                                       | 17.89      |
| DER                                       | 12.95      |
| ENE 1 Assessment - Dwelling Emission Rate |            |

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## Total Energy Type CO<sub>2</sub> Emissions for Codes Levels 1 - 5

|  | %    | kg/m²/year | 1     |
|--|------|------------|-------|
| DER from SAP 2012 DER Worksheet                                      |      | 12.95      | (ZC1) |
| TER  |      | 17.89      |       |
| Residual CO2 emissions offset from biofuel CHP                       |      | 0          | (ZC5) |
| CO2 emissions offset from additional allowable electricty generation |      | 0          | (ZC7) |
| Total CO2 emissions offset from SAP Section 16 allowances            |      | 0          |       |
| DER accounting for SAP Section 16 allowances                         |      | 12.95      |       |
| % improvement DER/TER  | 27.6 |            |       |
|  |      |            |       |

## Total Energy Type CO2 Emissions for Codes Levels 6

|   | kg/m²/year |       |
|---|------------|-------|
| DER accounting for SAP Section 16 allowances  | 12.95      | (ZC1) |
| CO2 emissions from appliances, equation (L14) | 16.96      | (ZC2) |
| CO2 emissions from cooking, equation (L16)    | 2.72       | (ZC3) |
| Net CO2 emissions                             | 36         | (ZC8) |

## Result:

## Credits awarded for ENE 1 = 3.6

Code Level = 4

### ENE 2 - Fabric energy Efficiency

## Fabric energy Efficiency: 46.36

### Credits awarded for ENE 2 = 3.5

ENE 7 - Low or Zero Carbon (LZC) Technologies

### **Reduction in CO2 Emissions**

|                             | %     | kg/m²/year |  |
|-----------------------------|-------|------------|--|
| Standard Case CO2 emissions |       | 40.63      |  |
| Standard DER                |       | 20.96      |  |
| Actual Case CO2 emissions   |       | 34.36      |  |
| Actual DER                  |       | 14.69      |  |
| Reduction in CO2 emissions  | 15.43 |            |  |

### Credits awarded for ENE 7 = 2

Technologies eligible to contribute to achieving the requirements of this issue must produce energy from renewable sources and meet all other ancillary requirements as defined by Directive 2009/28/EC of the European Parliament and of the Council of 23 April 2009 on the promotion of the use of energy from renewable sources and amending and subsequently repealing Directives 2001/77/EC and 2003/30/EC.

The following requirements must also be met:

• Where not provided by accredited external renewables there must be a direct supply of energy produced to the dwelling under assessment.

• Where covered by the Microgeneration Certification Scheme (MCS), technologies under 50kWe or 300kWth must be certified.

• Combined Heat and Power (CHP) schemes above 50kWe must be certified under the CHPQA standard.

• All technologies must be accounted for by SAP.

CHP schemes fuelled by mains gas are eligible to contribute to performance against this issue. Where these schemes are above 50kWe they must be certified under the CHPQA.

It is the responsibly of the Accredited OCDEA and Code Assessor to ensure all technologies use in the calculation are appropriate before awarding credits.

# **Predicted Energy Assessment**



| A-1-05<br>49-51 Beulah Hill |  |
|-----------------------------|--|
| Sada Unit Ref: A1-A11       |  |

Dwelling type: Date of assessment: Produced by: Total floor area: Mid floor Flat 12 March 2019 Aymon Winter 61.7 m<sup>2</sup>

This is a Predicted Energy Assessment for a property which is not yet complete. It includes a predicted energy rating which might not represent the final energy rating of the property on completion. Once the property is completed, an Energy Performance Certificate is required providing information about the energy performance of the completed property.

Energy performance has been assessed using the SAP 2012 methodology and is rated in terms of the energy use per square metre of floor area, energy efficiency based on fuel costs and environmental impact based on carbon dioxide (CO2) emissions.

#### **Energy Efficiency Rating** Environmental Impact (CO<sub>2</sub>) Rating Very energy efficient - lower running costs Very environmentally friendly - lower CO2 emissions (92 plus) 🖄 (92 plus) 🛕 91 В B (81-91) (81-91) 83 C C (69-80)(69-80) D D (55-68)(55-68)E Ξ (39-54)(39-54)F F (21 - 38)(21-38) G G (1-20)(1-20) Not energy efficient - higher running costs Not environmentally friendly - higher CO2 emissions **EU** Directive **EU** Directive **England & Wales England & Wales** 2002/91/EC 2002/91/EC

The energy efficiency rating is a measure of the overall efficiency of a home. The higher the rating the more energy efficient the home is and the lower the fuel bills are likely to be. The environmental impact rating is a measure of a home's impact on the environment in terms of carbonn dioxide (CO2) emissions. The higher the rating the less impact it has on the environment.

# **SAP** Input



### Property Details: 01-19-73120 A-1-05 PL1

| Address:<br>Located in:<br>Region: | A-1-05, 49-51 Beulah Hill<br>England<br>Thames valley |
|------------------------------------|---|
| UPRN:                              |   |
| Date of assessment:                | 12 March 2019   |
| Date of certificate:               | 25 March 2019   |
| Assessment type:                   | New dwelling design stage                             |
| Transaction type:                  | New dwelling  |
| Tenure type:                       | Unknown   |
| Related party disclosure:          | No related party                                      |
| Thermal Mass Parameter:            | Calculated 103.32                                     |
| Water use <= 125 litres/person/da  | ay: True  |
| PCDF Version:                      | 440   |

#### Property description:

| Dwelling type:<br>Detachment:            | Flat  |                |
|--|---|----------------|
| Year Completed:                          | 2013  |                |
| Floor Location:                          | Floor area:   |                |
|  |   | Storey height: |
| Floor 0                                  | 61.7 m <sup>2</sup>                                 | 2.56 m         |
| Living area:<br>Front of dwelling faces: | 26.05 m <sup>2</sup> (fraction 0.422)<br>North East |                |

### Opening types:

| opening cypesi    |              |                  |              |                 |        |                 |
|-------------------|--------------|------------------|--------------|-----------------|--------|-----------------|
| Name:             | Source:      | Туре:            | Glazing:     |                 | Argon: | Frame:          |
| Front Door        | Manufacturer | Solid            |              |                 |        | PVC-U           |
| Rear Elev         | SAP 2012     | Windows          | low-E, En =  | 0.05, soft coat | Yes    | Metal           |
| Rear Elev Balcony | SAP 2012     | Windows          | low-E, En =  | 0.05, soft coat | Yes    | Metal           |
| Side Elev         | SAP 2012     | Windows          | low-E, En =  | 0.05, soft coat | Yes    | Metal           |
| Name:             | Gap:         | Frame Fact       | or: g-value: | U-value:        | Area:  | No. of Openings |
| Front Door        | mm           | 0.7              | 0            | 1.4             | 2.12   | 1               |
| Rear Elev         | 16mm or more | 0.8              | 0.4          | 1.4             | 8.1    | 1               |
| Rear Elev Balcony | 16mm or more | 0.8              | 0.4          | 1.4             | 6.41   | 1               |
| Side Elev         | 16mm or more | 0.8              | 0.4          | 1.4             | 6.1    | 1               |
| Name:             | Type-Name:   | Location:        | Orient:      |                 | Width: | Height:         |
| Front Door        |              | Wall to Corridor | North East   |                 | 0      | 0               |
| Rear Elev         |              | External Wall    | South West   |                 | 0      | 0               |
| Rear Elev Balcony |              | External Wall    | South West   |                 | 2.68   | 2.39            |
| Side Elev         |              | External Wall    | North West   |                 | 0      | 0               |
|                   |              |                  |              |                 |        |                 |

Overshading:

Opaque Elements:

Average or unknown

| Туре:            | Gross area: | Openings: | Net area: | U-value: | Ru value: | Curtain wall: | Kappa: |
|------------------|-------------|-----------|-----------|----------|-----------|---------------|--------|
| External Element | <u>S</u>    |           |           |          |           |               |        |
| External Wall    | 60.77       | 20.61     | 40.16     | 0.13     | 0         | False         | 14     |
| Wall to Corridor | 16.38       | 2.12      | 14.26     | 0.26     | 0.43      | False         | 14     |
| Internal Element | <u>s</u>    |           |           |          |           |               |        |
| Iw Stud          | 116.48      |           |           |          |           |               | 9      |
| Party Elements   |             |           |           |          |           |               |        |
| Party Wall       | 12.29       |           |           |          |           |               | 20     |
| Party Ceiling    | 61.7        |           |           |          |           |               | 30     |

# **SAP Input**



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| Thermal bridges:   | User-defined (individual PSI-values) Y-Value = $0.1263$ LengthPsi-value10 $0.3$ E2Other lintels (including other steel lintels) $6.31$ $0.04$ E3Sill $26.98$ $0.05$ E4Jamb $60.28$ $0.07$ E7Party floor between dwellings (in blocks of flats) $10.24$ $0.09$ E16Corner (normal) $5.12$ $-0.09$ E17Corner (inverted – internal area greater than external area) $2.56$ $0.12$ E25Staggered party wall between dwellings c $9.6$ 0P3Intermediate floor between dwellings (in blocks of flats)   |
|--|--|
| Ventilation:   |  |
| Pressure test:<br>Ventilation:<br>Number of chimneys:<br>Number of open flues:<br>Number of fans:<br>Number of passive stacks:<br>Number of sides sheltered:<br>Pressure test: | Yes (As designed)<br>Centralised whole house extract<br>Number of wet rooms: Kitchen + 2<br>Ductwork: , rigid<br>Approved Installation Scheme: False<br>0<br>0<br>0<br>0<br>2<br>5   |
| Main heating system:   |  |
| Main heating system:   | <ul> <li>Boiler systems with radiators or underfloor heating</li> <li>Gas boilers and oil boilers</li> <li>Fuel: mains gas</li> <li>Info Source: Boiler Database</li> <li>Database: (rev 440, product index 017558) Efficiency: Winter 86.7 % Summer: 90.0</li> <li>Brand name: Worcester</li> <li>Model: Greenstar</li> <li>Model qualifier: 34CDi Classic ErP</li> <li>(Combi boiler)</li> <li>Systems with radiators</li> <li>Central heating pump : 2013 or later</li> <li>Design flow temperature: Unknown</li> <li>Boiler interlock: Yes</li> <li>Delayed start</li> </ul> |
| Main heating Control:  |  |
| Main heating Control:  | Programmer, room thermostat and TRVs<br>Control code: 2106   |
| Secondary heating system:  |  |
| Secondary heating system:  | None   |
| Water heating:<br>Water heating:<br>Others:  | From main heating system<br>Water code: 901<br>Fuel :mains gas<br>No hot water cylinder<br>Solar panel: False  |
| Electricity tariff:<br>In Smoke Control Area:  | Standard Tariff<br>Unknown   |

Party Floor

Thermal bridges:

61.7



# **SAP** Input

Conservatory: Low energy lights: Terrain type: EPC language: Wind turbine: Photovoltaics: No conservatory 100% Low rise urban / suburban English No <u>Photovoltaic 1</u> Installed Peak power: 0.98 Tilt of collector: Horizontal Overshading: None or very little Collector Orientation: South No

Assess Zero Carbon Home:



|   |                      |                           | User D      | etails:              |              |               |                        |             |                                 |      |
|---|----------------------|---------------------------|-------------|----------------------|--------------|---------------|------------------------|-------------|---------------------------------|------|
| Assessor Name:  | Aymon Wi             | nter                      |             | Strom                | a Num        | ber:          |                        | STRO        | 014511                          |      |
| Software Name:  | Stroma FS            | AP 2012                   |             | Softwa               | are Ver      | rsion:        |                        | Versio      | n: 1.0.4.16                     |      |
|   |                      | F                         | Property .  | Address              | 01-19-7      | 73120 A·      | -1-05 PL               | .1          |                                 |      |
| Address :   |                      | 51 Beulah Hill            |             |                      |              |               |                        |             |                                 |      |
| 1. Overall dwelling dime                                  | ensions:             |                           |             |                      |              |               |                        |             |                                 |      |
| Ground floor  |                      |                           |             | <b>a(m²)</b><br>61.7 | (1a) x       | <b>Av. He</b> | i <b>ght(m)</b><br>.56 | (2a) =      | Volume(m <sup>3</sup><br>157.95 | (3a) |
| Total floor area TFA = (1                                 | la)+(1b)+(1c)+       | (1d)+(1e)+(1              | n) 🦲        | 61.7                 | (4)          |               |                        |             |                                 |      |
| Dwelling volume   |                      |                           |             |                      | (3a)+(3b)    | )+(3c)+(3d    | )+(3e)+                | .(3n) =     | 157.95                          | (5)  |
| 2. Ventilation rate:                                      |                      |                           |             |                      |              |               |                        |             |                                 |      |
| Number of chimneys  | main<br>heating<br>0 | seconda<br>heating<br>+ 0 | ry<br>] + [ | other<br>0           | ] = [        | <b>total</b>  | x 4                    | 40 =        | m <sup>3</sup> per hou          | (6a) |
| Number of open flues                                      | 0                    | + 0                       | <u>_</u>    | 0                    | 」<br>] = 「   | 0             | x 2                    | 20 =        | 0                               | (6b) |
| Number of intermittent fa                                 |                      |                           |             | -                    |              | 0             | x 1                    | 10 =        | 0                               | (7a) |
| Number of passive vents                                   |                      |                           |             |                      |              | -             |                        | 10 =        | -                               | 4    |
|   |                      |                           |             |                      |              | 0             |                        | 10 =        | 0                               | (7b) |
| Number of flueless gas f                                  | ires                 |                           |             |                      |              | 0             |                        | +0 –        | 0                               | (7c) |
|   |                      |                           |             |                      |              |               |                        | Air ch      | anges per ho                    | our  |
| Infiltration due to chimne                                | eys, flues and fa    | ans = (6a)+(6b)+(         | 7a)+(7b)+(  | 7c) =                | Г            | 0             |                        | ÷ (5) =     | 0                               | (8)  |
| If a pressurisation test has                              | -                    |                           |             |                      | continue fro |               |                        | (- <i>Y</i> |                                 |      |
| Number of storeys in t                                    | the dwelling (na     | 3)                        |             |                      |              |               |                        |             | 0                               | (9)  |
| Additional infiltration                                   |                      |                           |             |                      |              |               | [(9)-                  | 1]x0.1 =    | 0                               | (10) |
| Structural infiltration: (<br>if both types of wall are p | present, use the va  | lue corresponding t       |             |                      |              | uction        |                        |             | 0                               | (11) |
| deducting areas of open<br>If suspended wooden            | •                    |                           | ).1 (seale  | ed). else            | enter 0      |               |                        |             | 0                               | (12) |
| If no draught lobby, er                                   |                      | . ,                       | ,           | ,,                   | -            |               |                        |             | 0                               | (13) |
| Percentage of window                                      | s and doors dr       | aught stripped            |             |                      |              |               |                        | -           | 0                               | (14) |
| Window infiltration                                       |                      |                           |             | 0.25 - [0.2          | x (14) ÷ 1   | = [00         |                        |             | 0                               | (15) |
| Infiltration rate   |                      |                           |             | (8) + (10)           | + (11) + (1  | 2) + (13) -   | + (15) =               |             | 0                               | (16) |
| Air permeability value                                    |                      |                           |             |                      |              | etre of e     | nvelope                | area        | 5                               | (17) |
| If based on air permeabi                                  | •                    |                           |             |                      |              |               | ,                      |             | 0.25                            | (18) |
| Air permeability value applie<br>Number of sides shelter  |                      | on test has been do       | ne or a deg | gree air pe          | rmeability   | is being us   | sed                    |             | 2                               | (19) |
| Shelter factor  | 54                   |                           |             | (20) = 1 -           | [0.075 x (1  | 9)] =         |                        |             | 0.85                            | (10) |
| Infiltration rate incorpora                               | ting shelter fac     | tor                       |             | (21) = (18           | ) x (20) =   |               |                        |             | 0.21                            | (21) |
| Infiltration rate modified                                | for monthly wir      | nd speed                  |             |                      |              |               |                        | '           |                                 |      |
| Jan Feb   | Mar Apr              | May Jun                   | Jul         | Aug                  | Sep          | Oct           | Nov                    | Dec         |                                 |      |
| Monthly average wind sp                                   | peed from Tabl       | e 7                       |             |                      |              |               |                        |             |                                 |      |
| (22)m= 5.1 5  | 4.9 4.4              | 4.3 3.8                   | 3.8         | 3.7                  | 4            | 4.3           | 4.5                    | 4.7         |                                 |      |
| Wind Factor (22a)m = (2                                   | 22)m ÷ 4             |                           |             |                      |              |               |                        |             |                                 |      |
| (22a)m= 1.27 1.25   | 1.23 1.1             | 1.08 0.95                 | 0.95        | 0.92                 | 1            | 1.08          | 1.12                   | 1.18        |                                 |      |
|   |                      |                           |             |                      |              |               |                        |             |                                 |      |



| Adjust             | ed infiltr | ation rat    | e (allowi                  | ng for sl   | nelter an   | d wind s       | speed)     | = (21a) >    | (22a)m           |              |             |                    |            |             |       |
|--------------------|------------|--------------|----------------------------|-------------|-------------|----------------|------------|--------------|------------------|--------------|-------------|--------------------|------------|-------------|-------|
|                    | 0.27       | 0.27         | 0.26                       | 0.23        | 0.23        | 0.2            | 0.2        | 0.2          | 0.21             | 0.23         | 0.24        | 0.25               |            |             |       |
|                    |            |              | change i                   | rate for t  | he appli    | cable ca       | se         | •            |                  | •            | -           | •                  |            |             | -     |
|                    |            | al ventila   |                            |             |             | /              |            |              |                  |              |             |                    | 0.5        | i           | (23a) |
|                    |            |              |                            |             |             |                |            |              | erwise (23b      | o) = (23a)   |             |                    | 0.5        | ;           | (23b) |
| If bala            | anced witl | n heat reco  | overy: effic               | iency in %  | allowing f  | or in-use f    | actor (fro | om Table 4   | h) =             |              |             |                    | 0          |             | (23c) |
| a) lf              | balance    | ed mecha     | anical ve                  | ntilation   | with he     | at recove      | ery (M\    | /HR) (24     | a)m = (2         | 2b)m + (     | 23b) × [    | 1 – (23c)          | ÷ 100]     |             |       |
| (24a)m=            | 0          | 0            | 0                          | 0           | 0           | 0              | 0          | 0            | 0                | 0            | 0           | 0                  |            |             | (24a) |
| b) lf              | balance    | ed mecha     | anical ve                  | entilation  | without     | heat rec       | covery     | (MV) (24     | b)m = (2         | 2b)m + (     | 23b)        |                    |            |             |       |
| (24b)m=            | 0          | 0            | 0                          | 0           | 0           | 0              | 0          | 0            | 0                | 0            | 0           | 0                  |            |             | (24b) |
| c) If              | whole h    | ouse ex      | tract ven                  | tilation of | or positiv  | e input        | ventilat   | ion from     | outside          |              |             |                    |            |             |       |
|                    | if (22b)r  | n < 0.5 ×    | < (23b), t                 | hen (24     | c) = (23b   | ); other       | wise (2    | 4c) = (22    | 2b) m + 0        | .5 × (23k    | o)          |                    |            |             |       |
| (24c)m=            | 0.52       | 0.52         | 0.51                       | 0.5         | 0.5         | 0.5            | 0.5        | 0.5          | 0.5              | 0.5          | 0.5         | 0.5                |            |             | (24c) |
| ,                  |            |              | on or wh<br>en (24d)       |             |             |                |            |              | loft<br>22b)m² x | 0.5]         |             |                    |            |             |       |
| (24d)m=            | 0          | 0            | 0                          | 0           | 0           | 0              | 0          | 0            | 0                | 0            | 0           | 0                  |            |             | (24d) |
| Effe               | ctive air  | change       | rate - er                  | nter (24a   | ı) or (24t  | o) or (24      | c) or (2   | 4d) in bo    | ox (25)          | •            |             | •                  |            |             |       |
| (25)m=             | 0.52       | 0.52         | 0.51                       | 0.5         | 0.5         | 0.5            | 0.5        | 0.5          | 0.5              | 0.5          | 0.5         | 0.5                |            |             | (25)  |
| 0.11               |            |              |                            |             | I           | I              | •          | 1            | -1               | 1            |             | <u> </u>           |            |             |       |
|                    |            |              | eat loss p                 |             |             |                |            |              |                  | A \/ 11      |             |                    |            |             |       |
| ELEN               | /IEN I     | Gros<br>area |                            | Openir<br>m | igs<br>1²   | Net Ar<br>A ,r |            | U-va<br>W/m  |                  | A X U<br>(W/ |             | k-value<br>kJ/m²·ł |            | A X<br>kJ/K |       |
| Doors              |            |              |                            |             |             | 2.12           | ×          | 1.4          | =                | 2.968        |             |                    |            |             | (26)  |
| Windo              | ws Type    | e 1          |                            |             |             | 8.1            | ×          | 1/[1/( 1.4 ) | + 0.04] =        | 10.74        |             |                    |            |             | (27)  |
| Windo              | ws Type    | e 2          |                            |             |             | 6.41           | ×          | 1/[1/( 1.4 ) | + 0.04] =        | 8.5          |             |                    |            |             | (27)  |
| Windo              | ws Type    | e 3          |                            |             |             | 6.1            | ×          | 1/[1/( 1.4 ) | + 0.04] =        | 8.09         |             |                    |            |             | (27)  |
| Walls <sup>·</sup> | Type1      | 60.7         | 7                          | 20.6        | 1           | 40.16          | 3 ×        | 0.13         | 3 =              | 5.22         |             | 14                 |            | 562.24      | (29)  |
| Walls <sup>·</sup> | Type2      | 16.3         | 38                         | 2.12        | 2           | 14.26          | ×          | 0.23         | 3 =              | 3.33         | i F         | 14                 | <b>i</b> F | 199.64      | (29)  |
| Total a            | area of e  | lements      |                            | L           |             | 77.15          | 5          |              |                  |              | I           |                    |            |             | (31)  |
| Party v            | wall       |              |                            |             |             | 12.29          | ) x        | 0            | =                | 0            |             | 20                 |            | 245.8       | (32)  |
| Party f            | loor       |              |                            |             |             | 61.7           |            |              |                  |              | i           | 40                 | <b>=</b>   | 2468        | (32a) |
| Party of           | ceiling    |              |                            |             |             | 61.7           |            |              |                  |              | ĺ           | 30                 | Ξ F        | 1851        | (32b) |
| Interna            | al wall ** |              |                            |             |             | 116.4          | 8          |              |                  |              | Ī           | 9                  |            | 048.32      | (32c) |
|                    |            |              | ows, use e<br>sides of in  |             |             |                | lated usir | ng formula   | 1/[(1/U-vali     | ue)+0.04] a  | as given in | paragraph          | 3.2        |             | _     |
| Fabric             | heat los   | s, W/K       | = S (A x                   | U)          |             |                |            | (26)(3       | 0) + (32) =      |              |             |                    | 38.8       | 35          | (33)  |
| Heat c             | apacity    | Cm = S(      | (Axk)                      |             |             |                |            |              | ((28).           | (30) + (3    | 2) + (32a). | (32e) =            | 637        | 5           | (34)  |
| Therm              | al mass    | parame       | ter (TMF                   | • = Cm -    | + TFA) ir   | n kJ/m²K       | ,          |              | = (34            | ) ÷ (4) =    |             |                    | 103.       | 32          | (35)  |
|                    | -          |              | ere the de<br>tailed calcu |             | construct   | ion are noi    | t known j  | precisely th | ne indicativo    | e values of  | TMP in T    | able 1f            |            |             | -     |
| Therm              | al bridg   | es : S (L    | x Y) cal                   | culated     | using Ap    | pendix I       | K          |              |                  |              |             |                    | 9.7        | 4           | (36)  |
|                    |            |              | are not kn                 | own (36) :  | = 0.15 x (3 | 1)             |            |              |                  |              |             |                    |            |             | -     |
| Total f            | abric he   | at loss      |                            |             |             |                |            |              | (33) +           | + (36) =     |             |                    | 48.5       | 59          | (37)  |



| Ventila                                  | tion hea                       | at loss c                           | alculate             | d monthl  | у                        |                         |                     | _          | (38)m        | = 0.33 × (             | (25)m x (5)                           |         |        |              |
|--|--------------------------------|-------------------------------------|----------------------|---|--------------------------|-------------------------|---------------------|------------|--------------|------------------------|---------------------------------------|---------|--------|--------------|
|  | Jan                            | Feb                                 | Mar                  | Apr   | May                      | Jun                     | Jul                 | Aug        | Sep          | Oct                    | Nov                                   | Dec     |        |              |
| (38)m=                                   | 27.15                          | 26.88                               | 26.6                 | 26.06   | 26.06                    | 26.06                   | 26.06               | 26.06      | 26.06        | 26.06                  | 26.06                                 | 26.06   |        | (38)         |
| Heat tr                                  | ansfer o                       | coefficie                           | nt, W/K              |   | -                        | -                       | -                   | -          | (39)m        | = (37) + (3            | 38)m                                  |         |        |              |
| (39)m=                                   | 75.74                          | 75.47                               | 75.19                | 74.65   | 74.65                    | 74.65                   | 74.65               | 74.65      | 74.65        | 74.65                  | 74.65                                 | 74.65   |        |              |
| Heat lo                                  | oss para                       | ameter (I                           | HLP), W              | //m²K   | •                        | -                       | -                   | -          |              | Average =<br>= (39)m ÷ | Sum(39)₁.<br>· (4)                    | 12 /12= | 74.86  | (39)         |
| (40)m=                                   | 1.23                           | 1.22                                | 1.22                 | 1.21  | 1.21                     | 1.21                    | 1.21                | 1.21       | 1.21         | 1.21                   | 1.21                                  | 1.21    |        |              |
| Numbe                                    | er of day                      | /s in mo                            | nth (Tab             | ble 1a)   | •                        |                         |                     |            | ,            | Average =              | Sum(40) <sub>1.</sub>                 | 12 /12= | 1.21   | (40)         |
|  | Jan                            | Feb                                 | Mar                  | Apr   | May                      | Jun                     | Jul                 | Aug        | Sep          | Oct                    | Nov                                   | Dec     |        |              |
| (41)m=                                   | 31                             | 28                                  | 31                   | 30  | 31                       | 30                      | 31                  | 31         | 30           | 31                     | 30                                    | 31      |        | (41)         |
|  | •                              |                                     |                      |   |                          |                         |                     |            |              |                        |                                       |         |        |              |
| 4. Wa                                    | ater hea                       | ting ene                            | rav reau             | irement:  |                          |                         |                     |            |              |                        |                                       | kWh/ye  | ear:   |              |
| if TF<br>if TF<br>Annua<br><i>Reduce</i> | A > 13.<br>A £ 13.<br>I averag | 9, N = 1<br>je hot wa<br>al average | + 1.76 x<br>ater usa | x [1 - exp<br>ge in litre<br><sup>r</sup> usage by<br>er day (all w | es per da<br>5% if the c | ay Vd,av<br>dwelling is | erage =<br>designed | (25 x N)   | + 36         |                        | .9)                                   | 03      |        | (42)<br>(43) |
|  | Jan                            | Feb                                 | Mar                  | Apr   | May                      | Jun                     | Jul                 | Aug        | Sep          | Oct                    | Nov                                   | Dec     |        |              |
| Hot wate                                 | er usage i                     | n litres pe                         | r day for e          | ach month   | Vd,m = fa                | ctor from               | Table 1c x          | (43)       |              |                        |                                       |         |        |              |
| (44)m=                                   | 90.63                          | 87.34                               | 84.04                | 80.75   | 77.45                    | 74.16                   | 74.16               | 77.45      | 80.75        | 84.04                  | 87.34                                 | 90.63   |        |              |
| Energy o                                 | content of                     | <sup>f</sup> hot water              | r used - ca          | lculated m  | onthly = 4.              | 190 x Vd,r              | m x nm x E          | DTm / 3600 |              |                        | m(44) <sub>112</sub> =<br>ables 1b, 1 |         | 988.74 | (44)         |
| (45)m=                                   | 134.41                         | 117.55                              | 121.31               | 105.76  | 101.48                   | 87.57                   | 81.14               | 93.11      | 94.23        | 109.81                 | 119.87                                | 130.17  |        |              |
| lf instan                                | taneous v                      | vater heat                          | ing at poin          | nt of use (no   | o hot wate               | r storage),             | enter 0 in          | boxes (46  |              | Total = Su             | m(45) <sub>112</sub> =                | :       | 1296.4 | (45)         |
|  | 20.16                          |                                     | 18.2                 | 15.86   | 15.22                    | 13.14                   | 12.17               | 13.97      | 14.13        | 16.47                  | 17.98                                 | 19.53   |        | (46)         |
|  | storage<br>e volum             |                                     | ) includi            | ng any s  | olar or W                | WHRS                    | storage             | within sa  | ame ves      | sel                    |                                       | 0       |        | (47)         |
| Otherv<br>Water                          | vise if no<br>storage          | o stored<br>loss:                   | hot wat              | ank in dw<br>er (this ir  | ncludes i                | instantar               | neous co            | . ,        | ers) ente    | er '0' in (            | 47)                                   |         |        |              |
| a) If m                                  | nanufact                       | turer's d                           | eclared              | loss fact   | or is kno                | wn (kWł                 | n/day):             |            |              |                        |                                       | 0       |        | (48)         |
| Tempe                                    | erature f                      | actor fro                           | om Table             | e 2b  |                          |                         |                     |            |              |                        |                                       | 0       |        | (49)         |
| b) If m                                  | nanufact                       | turer's d                           | eclared              | e, kWh/ye<br>cylinder   | loss fact                |                         | known:              | (48) x (49 | ) =          |                        |                                       | 0       |        | (50)         |
|  |                                | -                                   |                      | rom Tab   | le 2 (kW                 | h/litre/da              | ay)                 |            |              |                        |                                       | 0       |        | (51)         |
|  | •                              | from Ta                             | see sect             | ion 4.3   |                          |                         |                     |            |              |                        |                                       | ]       |        | (52)         |
|  |                                |                                     | om Table             | e 2b  |                          |                         |                     |            |              |                        |                                       | 0<br>0  |        | (52)<br>(53) |
|  |                                |                                     |                      | ə, kWh/y  | ear                      |                         |                     | (47) x (51 | ) x (52) x ( | 53) =                  |                                       |         |        | (54)         |
| •••                                      |                                | (54) in (                           | -                    | ο, ιτνντι/y   | Jul                      |                         |                     | (1) (01    | , ~ (02) ^ ( | ~~,                    |                                       | 0       |        | (54)         |
|  | . ,                            | . , .                               |                      | for each  | month                    |                         |                     | ((56)m = ( | (55) × (41)  | m                      |                                       | -       |        | ()           |
| (56)m=                                   | 0                              | 0                                   | 0                    | 0   | 0                        | 0                       | 0                   | 0          | 0            | 0                      | 0                                     | 0       |        | (56)         |
|  |                                | I                                   | 1                    |   |                          | I                       | I                   | I          | I            | I                      |                                       |         |        |              |



| If cylinde | er contain | s dedicate           | d solar sto | orage, (57) | m = (56)m  | x [(50) – ( | H11)] ÷ (5  | 0), else (5  | 7)m = (56)    | )m where (  | H11) is fro   | m Append    | ix H          |      |
|------------|------------|----------------------|-------------|-------------|------------|-------------|-------------|--------------|---------------|-------------|---------------|-------------|---------------|------|
| (57)m=     | 0          | 0                    | 0           | 0           | 0          | 0           | 0           | 0            | 0             | 0           | 0             | 0           |               | (57) |
| Primar     | y circui   | t loss (ar           | nual) fro   | om Table    | e 3        |             | _           |              |               | -           |               | 0           |               | (58) |
| Primar     | y circui   | t loss cal           | culated     | for each    | month (    | 59)m = (    | (58) ÷ 36   | 65 × (41)    | m             |             |               |             |               |      |
| (mo        | dified by  | / factor fi          | rom Tab     | le H5 if t  | here is s  | olar wat    | er heatii   | ng and a     | cylinde       | r thermo    | stat)         |             |               |      |
| (59)m=     | 0          | 0                    | 0           | 0           | 0          | 0           | 0           | 0            | 0             | 0           | 0             | 0           |               | (59) |
| Combi      | loss ca    | lculated             | for each    | month (     | (61)m =    | (60) ÷ 36   | 65 × (41)   | )m           |               |             |               |             |               |      |
| (61)m=     | 35.72      | 32.23                | 35.64       | 34.44       | 35.55      | 34.36       | 35.48       | 35.53        | 34.41         | 35.61       | 34.52         | 35.7        |               | (61) |
| Total h    | neat req   | uired for            | water h     | eating ca   | alculated  | l for eacl  | n month     | (62)m =      | 0.85 ×        | (45)m +     | (46)m +       | (57)m +     | (59)m + (61)m |      |
| (62)m=     | 170.13     | 149.79               | 156.95      | 140.2       | 137.03     | 121.93      | 116.63      | 128.64       | 128.63        | 145.42      | 154.38        | 165.87      |               | (62) |
| Solar DI   | -IW input  | calculated           | using App   | endix G or  | r Appendix | H (negativ  | ve quantity | /) (enter '0 | ' if no sola  | r contribut | ion to wate   | er heating) |               |      |
| (add a     | dditiona   | al lines if          | FGHRS       | and/or \    | NWHRS      | applies     | , see Ap    | pendix (     | G)            |             | _             | _           |               |      |
| (63)m=     | 0          | 0                    | 0           | 0           | 0          | 0           | 0           | 0            | 0             | 0           | 0             | 0           |               | (63) |
| Output     | t from w   | ater hea             | ter         |             |            |             |             |              |               | _           |               |             |               |      |
| (64)m=     | 170.13     | 149.79               | 156.95      | 140.2       | 137.03     | 121.93      | 116.63      | 128.64       | 128.63        | 145.42      | 154.38        | 165.87      |               | _    |
|            |            |                      |             |             |            |             |             | Outp         | out from w    | ater heate  | r (annual)₁   | 12          | 1715.6        | (64) |
| Heat g     | ains fro   | m water              | heating     | , kWh/m     | onth 0.2   | 5 ´ [0.85   | × (45)m     | + (61)m      | n] + 0.8 x    | x [(46)m    | + (57)m       | + (59)m     | ]             |      |
| (65)m=     | 53.62      | 47.15                | 49.24       | 43.77       | 42.63      | 37.71       | 35.85       | 39.84        | 39.93         | 45.41       | 48.48         | 52.21       |               | (65) |
| inclu      | ıde (57)   | m in calo            | culation    | of (65)m    | only if c  | ylinder i   | s in the o  | dwelling     | or hot w      | ater is fr  | om com        | munity h    | eating        |      |
| 5. Int     | ternal g   | ains (see            | e Table 5   | 5 and 5a    | ):         |             |             |              |               |             |               |             |               |      |
| Metab      | olic gair  | ns (Table            | e 5), Wat   | ts          |            |             |             |              |               |             |               |             |               |      |
|            | Jan        | Feb                  | Mar         | Apr         | May        | Jun         | Jul         | Aug          | Sep           | Oct         | Nov           | Dec         |               |      |
| (66)m=     | 121.76     | 121.76               | 121.76      | 121.76      | 121.76     | 121.76      | 121.76      | 121.76       | 121.76        | 121.76      | 121.76        | 121.76      |               | (66) |
| Lightin    | g gains    | (calcula             | ted in Ap   | opendix     | L, equat   | ion L9 oi   | r L9a), a   | lso see      | Table 5       |             |               |             |               |      |
| (67)m=     | 39.5       | 35.08                | 28.53       | 21.6        | 16.15      | 13.63       | 14.73       | 19.14        | 25.7          | 32.63       | 38.08         | 40.59       |               | (67) |
| Applia     | nces ga    | ins (calc            | ulated ir   | n Append    | dix L, eq  | uation L    | 13 or L1    | 3a), also    | see Ta        | ble 5       |               |             |               |      |
| (68)m=     | 264.5      | 267.24               | 260.33      | 245.6       | 227.01     | 209.55      | 197.88      | 195.13       | 202.05        | 216.77      | 235.36        | 252.83      |               | (68) |
| Cookir     | ng gains   | (calcula             | ited in A   | ppendix     | L, equat   | tion L15    | or L15a)    | ), also se   | e Table       | e 5         |               | _           |               |      |
| (69)m=     | 49.2       | 49.2                 | 49.2        | 49.2        | 49.2       | 49.2        | 49.2        | 49.2         | 49.2          | 49.2        | 49.2          | 49.2        |               | (69) |
| Pumps      | s and fa   | ns gains             | (Table \$   | 5a)         |            | -           | _           | -            | -             |             |               | -           |               |      |
| (70)m=     | 3          | 3                    | 3           | 3           | 3          | 3           | 3           | 3            | 3             | 3           | 3             | 3           |               | (70) |
| Losses     | s e.g. ev  | aporatio             | on (nega    | tive valu   | es) (Tab   | le 5)       |             |              |               | -           |               | _           |               |      |
| (71)m=     | -81.17     | -81.17               | -81.17      | -81.17      | -81.17     | -81.17      | -81.17      | -81.17       | -81.17        | -81.17      | -81.17        | -81.17      |               | (71) |
| Water      | heating    | gains (T             | able 5)     | -           |            | -           |             | •            | •             |             |               |             |               |      |
| (72)m=     | 72.07      | 70.16                | 66.19       | 60.8        | 57.3       | 52.37       | 48.19       | 53.55        | 55.46         | 61.04       | 67.34         | 70.17       |               | (72) |
| Total i    | nterna     | gains =              |             |             | •          | (66)        | m + (67)m   | n + (68)m +  | + (69)m +     | (70)m + (7  | 1)m + (72)    | m           |               |      |
| (73)m=     | 468.85     | 465.27               | 447.83      | 420.79      | 393.25     | 368.34      | 353.58      | 360.62       | 375.99        | 403.23      | 433.57        | 456.38      |               | (73) |
| 6. So      | lar gain   | s:                   | •           | •           | •          | •           |             | •            | •             | -           | •             |             |               |      |
| Solar g    | gains are  | calculated           | using sola  | r flux from | Table 6a   | and assoc   | iated equa  | tions to co  | onvert to th  | ne applicat | ole orientat  | ion.        |               |      |
| Orienta    |            | Access F<br>Table 6d |             | Area<br>m²  |            | Flu<br>Tal  | x<br>ole 6a | Т            | g_<br>able 6b | Т           | FF<br>able 6c |             | Gains<br>(W)  |      |

Table 6a



| Southwoote o              |      | 1 |      | 1 |        |   |     | 1 |     | 1          | r      | ٦    |
|---------------------------|------|---|------|---|--------|---|-----|---|-----|------------|--------|------|
| Southwest <sub>0.9x</sub> | 0.77 | X | 8.1  | X | 36.79  |   | 0.4 | Х | 0.8 | =          | 66.09  | (79) |
| Southwest <sub>0.9x</sub> | 0.77 | х | 6.41 | х | 36.79  |   | 0.4 | х | 0.8 | =          | 52.3   | (79) |
| Southwest <sub>0.9x</sub> | 0.77 | х | 8.1  | x | 62.67  |   | 0.4 | x | 0.8 | =          | 112.58 | (79) |
| Southwest <sub>0.9x</sub> | 0.77 | х | 6.41 | х | 62.67  |   | 0.4 | x | 0.8 | =          | 89.09  | (79) |
| Southwest <sub>0.9x</sub> | 0.77 | х | 8.1  | х | 85.75  |   | 0.4 | x | 0.8 | =          | 154.03 | (79) |
| Southwest <sub>0.9x</sub> | 0.77 | х | 6.41 | х | 85.75  |   | 0.4 | x | 0.8 | =          | 121.9  | (79) |
| Southwest <sub>0.9x</sub> | 0.77 | x | 8.1  | x | 106.25 |   | 0.4 | x | 0.8 | =          | 190.86 | (79) |
| Southwest <sub>0.9x</sub> | 0.77 | х | 6.41 | x | 106.25 |   | 0.4 | x | 0.8 | =          | 151.03 | (79) |
| Southwest <sub>0.9x</sub> | 0.77 | x | 8.1  | x | 119.01 |   | 0.4 | x | 0.8 | =          | 213.77 | (79) |
| Southwest <sub>0.9x</sub> | 0.77 | x | 6.41 | x | 119.01 |   | 0.4 | x | 0.8 | =          | 169.17 | (79) |
| Southwest <sub>0.9x</sub> | 0.77 | x | 8.1  | x | 118.15 |   | 0.4 | x | 0.8 | =          | 212.23 | (79) |
| Southwest <sub>0.9x</sub> | 0.77 | x | 6.41 | x | 118.15 |   | 0.4 | x | 0.8 | =          | 167.95 | (79) |
| Southwest <sub>0.9x</sub> | 0.77 | x | 8.1  | x | 113.91 |   | 0.4 | x | 0.8 | =          | 204.61 | (79) |
| Southwest <sub>0.9x</sub> | 0.77 | x | 6.41 | x | 113.91 |   | 0.4 | x | 0.8 | =          | 161.92 | (79) |
| Southwest <sub>0.9x</sub> | 0.77 | x | 8.1  | x | 104.39 |   | 0.4 | x | 0.8 | =          | 187.51 | (79) |
| Southwest <sub>0.9x</sub> | 0.77 | x | 6.41 | x | 104.39 |   | 0.4 | x | 0.8 | =          | 148.39 | (79) |
| Southwest <sub>0.9x</sub> | 0.77 | x | 8.1  | x | 92.85  |   | 0.4 | x | 0.8 | =          | 166.79 | (79) |
| Southwest <sub>0.9x</sub> | 0.77 | x | 6.41 | x | 92.85  |   | 0.4 | x | 0.8 | =          | 131.99 | (79) |
| Southwest <sub>0.9x</sub> | 0.77 | x | 8.1  | x | 69.27  |   | 0.4 | x | 0.8 | =          | 124.42 | (79) |
| Southwest <sub>0.9x</sub> | 0.77 | x | 6.41 | x | 69.27  |   | 0.4 | x | 0.8 | =          | 98.46  | (79) |
| Southwest <sub>0.9x</sub> | 0.77 | x | 8.1  | x | 44.07  | İ | 0.4 | x | 0.8 | <b>i</b> = | 79.16  | (79) |
| Southwest <sub>0.9x</sub> | 0.77 | x | 6.41 | x | 44.07  |   | 0.4 | x | 0.8 | =          | 62.65  | (79) |
| Southwest <sub>0.9x</sub> | 0.77 | x | 8.1  | x | 31.49  | ĺ | 0.4 | x | 0.8 | =          | 56.56  | (79) |
| Southwest <sub>0.9x</sub> | 0.77 | x | 6.41 | x | 31.49  | İ | 0.4 | x | 0.8 | <b>i</b> = | 44.76  | (79) |
| Northwest 0.9x            | 0.77 | x | 6.1  | x | 11.28  | x | 0.4 | x | 0.8 | <b>j</b> = | 15.26  | (81) |
| Northwest 0.9x            | 0.77 | x | 6.1  | x | 22.97  | x | 0.4 | x | 0.8 | =          | 31.07  | (81) |
| Northwest 0.9x            | 0.77 | x | 6.1  | x | 41.38  | x | 0.4 | x | 0.8 | <b>i</b> = | 55.97  | (81) |
| Northwest 0.9x            | 0.77 | x | 6.1  | x | 67.96  | x | 0.4 | x | 0.8 | =          | 91.93  | (81) |
| Northwest 0.9x            | 0.77 | x | 6.1  | x | 91.35  | x | 0.4 | x | 0.8 | =          | 123.57 | (81) |
| Northwest 0.9x            | 0.77 | x | 6.1  | x | 97.38  | x | 0.4 | x | 0.8 | =          | 131.74 | (81) |
| Northwest 0.9x            | 0.77 | x | 6.1  | x | 91.1   | х | 0.4 | x | 0.8 | =          | 123.24 | (81) |
| Northwest 0.9x            | 0.77 | x | 6.1  | x | 72.63  | x | 0.4 | x | 0.8 | =          | 98.25  | (81) |
| Northwest 0.9x            | 0.77 | x | 6.1  | × | 50.42  | x | 0.4 | x | 0.8 | =          | 68.21  | (81) |
| Northwest 0.9x            | 0.77 | x | 6.1  | x | 28.07  | x | 0.4 | x | 0.8 | =          | 37.97  | (81) |
| Northwest 0.9x            | 0.77 | x | 6.1  | x | 14.2   | x | 0.4 | x | 0.8 | =          | 19.2   | (81) |
| Northwest 0.9x            | 0.77 | x | 6.1  | x | 9.21   | x | 0.4 | x | 0.8 | =          | 12.46  | (81) |

| Solar g  | ains in   | watts, ca           | alculated   | for eacl  | h month     |           | -                    | (83)m = S | um(74)m . | (82)m  |        |        | _    |          |
|----------|-----------|---------------------|-------------|-----------|-------------|-----------|----------------------|-----------|-----------|--------|--------|--------|------|----------|
| (83)m=   | 133.66    | 232.73              | 331.9       | 433.82    | 506.51      | 511.91    | 489.77               | 434.15    | 366.98    | 260.85 | 161.01 | 113.78 |      | (83)     |
| Total g  | ains – iı | nternal a           | ind solar   | (84)m =   | = (73)m ·   | + (83)m   | , watts              |           |           |        |        |        |      |          |
| (84)m=   | 602.51    | 698                 | 779.74      | 854.6     | 899.76      | 880.25    | 843.35               | 794.76    | 742.97    | 664.08 | 594.58 | 570.17 |      | (84)     |
| 7. Me    | an inter  | nal temp            | erature     | (heating  | season      | )         |                      |           |           |        |        |        |      |          |
| Temp     | erature   | during h            | eating p    | eriods ir | n the livir | ng area t | from Tab             | ole 9, Th | 1 (°C)    |        |        |        | 21   | (85)     |
| Utilisa  | ation fac | tor for g           | ains for l  | iving are | ea, h1,m    | (see Ta   | ble 9a)              |           |           |        |        |        |      |          |
| Stroma I | SAP 201   | 2 v <b>Ersio</b> n: | 1.0.4.916 ( | SAP 9.92  | - http://ww | vw.stroma | . <sub>com</sub> lul | Aug       | Sep       | Oct    | Nov    | Dec    | Page | e 5 of 8 |



| (86)m=         | 0.92            | 0.88       | 0.83             | 0.74               | 0.62           | 0.49        | 0.37         | 0.4         | 0.58         | 0.77                  | 0.88                    | 0.92                   |          | (86)    |
|----------------|-----------------|------------|------------------|--------------------|----------------|-------------|--------------|-------------|--------------|-----------------------|-------------------------|------------------------|----------|---------|
| Mear           | interna         | l temper   | ature in         | living are         | ea T1 (fo      | ollow ste   | ps 3 to 7    | 7 in Table  | e 9c)        |                       |                         |                        |          |         |
| (87)m=         | 19.03           | 19.34      | 19.77            | 20.25              | 20.63          | 20.86       | 20.95        | 20.93       | 20.77        | 20.27                 | 19.57                   | 18.98                  |          | (87)    |
| Temp           | erature         | during h   | eating p         | periods ir         | n rest of      | dwelling    | from Ta      | able 9, Tl  | h2 (°C)      |                       |                         |                        |          |         |
| (88)m=         | 19.9            | 19.9       | 19.91            | 19.91              | 19.91          | 19.91       | 19.91        | 19.91       | 19.91        | 19.91                 | 19.91                   | 19.91                  |          | (88)    |
| Utilis         | ation fac       | tor for g  | ains for         | rest of d          | welling,       | h2,m (se    | e Table      | 9a)         |              |                       |                         |                        |          |         |
| (89)m=         | 0.9             | 0.86       | 0.8              | 0.71               | 0.57           | 0.42        | 0.28         | 0.32        | 0.51         | 0.74                  | 0.86                    | 0.91                   |          | (89)    |
| Mear           | interna         | l temper   | ature in         | the rest           | of dwelli      | ina T2 (f   | ollow ste    | eps 3 to 7  | 7 in Tabl    | e 9c)                 |                         |                        |          |         |
| (90)m=         | 18.14           | 18.44      | 18.85            | 19.31              | 19.64          | 19.83       | 19.89        | 19.88       | 19.77        | 19.34                 | 18.68                   | 18.1                   |          | (90)    |
|                |                 |            | <u> </u>         |                    | <u> </u>       |             | <u> </u>     |             | 1            | LA = Livin            | g area ÷ (4             | 4) =                   | 0.42     | (91)    |
| Moor           | interna         | l tomnor   | ature (fo        | or the wh          | olo dwo        | llina) = fl | Δ x T1       | + (1 – fL   | Δ) x T2      |                       |                         |                        |          |         |
| (92)m=         | 18.51           | 18.82      | 19.24            | 19.7               | 20.06          | 20.26       | 20.34        | 20.33       | 20.19        | 19.73                 | 19.06                   | 18.47                  |          | (92)    |
|                |                 |            |                  |                    |                |             |              | e 4e, whe   |              | opriate               |                         |                        |          |         |
| (93)m=         | 18.36           | 18.67      | 19.09            | 19.55              | 19.91          | 20.11       | 20.19        | 20.18       | 20.04        | 19.58                 | 18.91                   | 18.32                  |          | (93)    |
| 8. Sp          | ace hea         | iting requ | uirement         | i                  | 1              |             | 1            | <b>.</b>    |              |                       | <u> </u>                | <u> </u>               |          |         |
|                |                 |            |                  |                    |                | ned at ste  | ep 11 of     | Table 9     | o, so tha    | t Ti,m=(              | 76)m an                 | d re-calc              | ulate    |         |
| the u          |                 |            |                  | using Ta           |                |             |              |             |              |                       |                         |                        |          |         |
| LICE.          | Jan             | Feb        | Mar              | Apr                | May            | Jun         | Jul          | Aug         | Sep          | Oct                   | Nov                     | Dec                    | I        |         |
| (94)m=         | 0.88            | tor for g  | ains, nm<br>0.79 | 0.69               | 0.57           | 0.43        | 0.31         | 0.34        | 0.52         | 0.72                  | 0.84                    | 0.89                   |          | (94)    |
|                |                 |            |                  | 4)m x (84          |                | 0.43        | 0.31         | 0.34        | 0.52         | 0.72                  | 0.04                    | 0.09                   | 1        | (34)    |
| (95)m=         | 532.37          | 589        | 612.54           | 593.42             | 515.72         | 378.68      | 258.23       | 269.13      | 387.35       | 480.99                | 501.93                  | 509.91                 |          | (95)    |
|                |                 |            |                  | perature           |                |             | 200.20       | 200.10      | 001.00       | 100.00                | 001.00                  | 000.01                 |          | ()      |
| (96)m=         | 4.3             | 4.9        | 6.5              | 8.9                | 11.7           | 14.6        | 16.6         | 16.4        | 14.1         | 10.6                  | 7.1                     | 4.2                    |          | (96)    |
|                | Loss rate       | e for mea  | an interr        |                    | erature,       |             | L<br>=[(39)m | x [(93)m·   | L<br>_ (96)m | 1                     |                         |                        |          |         |
| (97)m=         | 1065.13         | î .        | 946.39           | 795.26             | 612.71         | 411.65      | 267.85       | 281.99      | 443.29       | 670.59                | 881.46                  | 1054.02                |          | (97)    |
| Spac           | e heatin        | g require  | ement fo         | r each n           | nonth, k       | Wh/mon      | th = 0.02    | 24 x [(97]  | )m – (95     | )m] x (4 <sup>-</sup> | 1)m                     |                        |          |         |
| (98)m=         | 396.38          | 302.4      | 248.38           | 145.33             | 72.16          | 0           | 0            | 0           | 0            | 141.07                | 273.26                  | 404.82                 |          |         |
|                |                 |            |                  |                    |                |             |              | Tota        | l per year   | (kWh/year             | .) = Sum(9              | 8) <sub>15,912</sub> = | 1983.79  | (98)    |
| Spac           | e heatin        | g require  | ement in         | kWh/m <sup>2</sup> | ²/year         |             |              |             |              |                       |                         |                        | 32.15    | (99)    |
| 9a. En         | erav rea        | uiremer    | nts – Ind        | ividual h          | eatina s       | vstems i    | ncludinc     | g micro-C   | CHP)         |                       |                         |                        |          |         |
|                | e heatii        |            |                  |                    | 5              | ,           |              |             |              |                       |                         |                        |          |         |
| Fract          | ion of sp       | bace hea   | at from s        | econdar            | y/supple       | mentary     | system       |             |              |                       |                         |                        | 0        | (201)   |
| Fract          | ion of sp       | bace hea   | at from n        | nain syst          | em(s)          |             |              | (202) = 1 - | - (201) =    |                       |                         |                        | 1        | (202)   |
| Fract          | ion of to       | tal heati  | ng from          | main sys           | stem 1         |             |              | (204) = (20 | 02) × [1 –   | (203)] =              |                         |                        | 1        | (204)   |
| Efficie        | ency of         | main spa   | ace heat         | ing syste          | em 1           |             |              |             |              |                       |                         |                        | 90       | (206)   |
|                | -               |            |                  | ementar            |                | a svsten    | ı. %         |             |              |                       |                         |                        | 0        | (208)   |
|                | -               | Feb        |                  |                    | -              |             | Jul          | Aug         | Sep          | Oct                   | Nov                     | Dee                    | kWh/ye   |         |
| Snac           | Jan<br>e heatin | <u> </u>   | Mar              | Apr<br>alculate    | May<br>d above | Jun         | Jui          | Aug         | Sep          | 001                   | Nov                     | Dec                    | Kvvii/ye | ai      |
| opao           | 396.38          | 302.4      | 248.38           | 145.33             | 72.16          | 0           | 0            | 0           | 0            | 141.07                | 273.26                  | 404.82                 |          |         |
| (211)n         |                 |            |                  | 1<br>100 ÷ (20     |                |             | I            | I           |              |                       | I                       | I                      |          | (211)   |
| (د ۱۱ <i>)</i> | 440.42          | 336        | 275.98           | 161.47             | 80.18          | 0           | 0            | 0           | 0            | 156.74                | 303.63                  | 449.79                 |          | (~ 1 1) |
|                | L               |            |                  | I                  |                | I           | <u> </u>     |             | -            |                       | 211) <sub>15,1012</sub> |                        | 2204.22  | (211)   |
|                |                 |            |                  |                    |                |             |              |             |              |                       |                         |                        | 4        |         |



Space heating fuel (secondary), kWh/month

| = {[(98)m x (201)] } x 100 ÷ (2                                       | 08)        |                 |                   |                      |            |             |                         |                         |                     | _                          |        |
|---|------------|-----------------|-------------------|----------------------|------------|-------------|-------------------------|-------------------------|---------------------|----------------------------|--------|
| (215)m= 0 0 0   | 0          | 0               | 0                 | 0                    | 0          | 0           | 0                       | 0                       | 0                   |                            | _      |
|   |            |                 |                   |                      | Tota       | ıl (kWh/yea | ar) =Sum(2              | 215) <sub>15,1012</sub> | =                   | 0                          | (215)  |
| Water heating   |            |                 |                   |                      |            |             |                         |                         |                     |                            |        |
| Output from water heater (cale<br>170.13 149.79 156.95                |            | oove)<br>137.03 | 121.93            | 116.63               | 128.64     | 128.63      | 145.42                  | 154.38                  | 165.87              | 1                          |        |
| Efficiency of water heater  |            |                 |                   |                      |            |             |                         |                         |                     | 86.7                       | (216)  |
| (217)m= 88.98 88.88 88.69   | 88.35      | 87.81           | 86.7              | 86.7                 | 86.7       | 86.7        | 88.29                   | 88.78                   | 89.02               |                            | (217)  |
| Fuel for water heating, kWh/m $(219)m = (64)m \times 100 \div (217)m$ |            |                 |                   |                      |            |             |                         |                         |                     | 1                          |        |
| (219)m = 191.19 168.53 176.96   | 1          | 156.05          | 140.64            | 134.52               | 148.38     | 148.37      | 164.7                   | 173.89                  | 186.34              | ]                          |        |
|   |            |                 |                   |                      | Tota       | I = Sum(2   | 19a) <sub>112</sub> =   |                         |                     | 1948.25                    | (219)  |
| Annual totals   |            |                 |                   |                      |            |             | k                       | Wh/year                 | ,                   | kWh/year                   | -      |
| Space heating fuel used, main   | n system   | 1               |                   |                      |            |             |                         |                         |                     | 2204.22                    |        |
| Water heating fuel used   |            |                 |                   |                      |            |             |                         |                         |                     | 1948.25                    |        |
| Electricity for pumps, fans and                                       | d electric | keep-ho         | t                 |                      |            |             |                         |                         |                     |                            |        |
| mechanical ventilation - bala   | nced, ext  | ract or p       | ositive i         | nput fror            | n outsid   | е           |                         |                         | 40.47               | ]                          | (230a) |
| central heating pump:   |            |                 |                   |                      |            |             |                         |                         | 30                  | Ī                          | (230c) |
| boiler with a fan-assisted flue                                       | Э          |                 |                   |                      |            |             |                         |                         | 45                  | ]                          | (230e) |
| Total electricity for the above,                                      | kWh/yea    | r               |                   |                      | sum        | of (230a).  | (230g) =                | :                       |                     | 115.47                     | (231)  |
| Electricity for lighting  |            |                 |                   |                      |            |             |                         |                         |                     | 279.01                     | (232)  |
| Electricity generated by PVs  |            |                 |                   |                      |            |             |                         |                         |                     | -745.28                    | (233)  |
| 10a. Fuel costs - individual h  | eating sy  | stems:          |                   |                      |            |             |                         |                         |                     |                            |        |
|   |            |                 | <b>Fu</b><br>kW   | <b>el</b><br>/h/year |            |             | <b>Fuel P</b><br>(Table |                         |                     | <b>Fuel Cost</b><br>£/year |        |
| Space heating - main system   | 1          |                 | (21               | 1) x                 |            |             | 3.4                     | 8                       | x 0.01 =            | 76.71                      | (240)  |
| Space heating - main system   | 2          |                 | (21;              | 3) x                 |            |             | 0                       | , i i                   | x 0.01 =            | 0                          | (241)  |
| Space heating - secondary   |            |                 | (21               | 5) x                 |            |             | 13.                     | 19                      | x 0.01 =            | 0                          | (242)  |
| Water heating cost (other fuel  | )          |                 | (219              | 9)                   |            |             | 3.4                     | 18                      | x 0.01 =            | 67.8                       | (247)  |
| Pumps, fans and electric keep   | o-hot      |                 | (23               | 1)                   |            |             | 13.                     | 19                      | x 0.01 =            | 15.23                      | (249)  |
| (if off-peak tariff, list each of (2<br>Energy for lighting           | 230a) to ( | 230g) se        | eparately<br>(232 |                      | licable a  | nd apply    | / fuel pri<br>13.       |                         | ding to<br>x 0.01 = | Table 12a<br>36.8          | (250)  |
| Additional standing charges (   | Table 12)  |                 |                   |                      |            |             |                         |                         |                     | 120                        | (251)  |
|   |            |                 | one               | e of (233) to        | o (235) x) |             | 13.                     | 10                      | x 0.01 =            | 0                          | (252)  |
| Appendix Q items: repeat line   | s (253) ai | nd (254)        |                   |                      |            |             | L                       | .~                      |                     | v                          |        |
| Total energy cost   | s (200) al | . ,             | (247) + (25       |                      | =          |             |                         |                         |                     | 316.54                     | (255)  |
| 11a. SAP rating - individual h  | neating sy | vstems          |                   |                      |            |             |                         |                         |                     |                            | _      |
| Energy cost deflator (Table 12  | 2)         |                 |                   |                      |            |             |                         |                         |                     | 0.40                       |        |
| LINGLY COST UCHALON (TADLE 12   | -)         |                 |                   |                      |            |             |                         |                         |                     | 0.42                       | (256)  |



| Energy cost factor (ECF) [(255) x (               | 256)] ÷ [(4) + 45.0] =    |                                      | 1.25 (2                         | 257) |
|---|---------------------------|--------------------------------------|---------------------------------|------|
| SAP rating (Section 12)                           |                           |                                      | 82.62 (2                        | 258) |
| 12a. CO2 emissions – Individual heating syster    | ms including micro-Cl     | HP                                   |                                 |      |
|   | <b>Energy</b><br>kWh/year | <b>Emission factor</b><br>kg CO2/kWh | <b>Emissions</b><br>kg CO2/year |      |
| Space heating (main system 1)                     | (211) x                   | 0.216 =                              | 476.11 (2                       | 261) |
| Space heating (secondary)                         | (215) x                   | 0.519 =                              | 0 (2                            | 263) |
| Water heating                                     | (219) x                   | 0.216 =                              | 420.82 (2                       | 264) |
| Space and water heating                           | (261) + (262) + (263)     | + (264) =                            | 896.93 (2                       | 265) |
| Electricity for pumps, fans and electric keep-hot | (231) x                   | 0.519 =                              | 59.93 (2                        | 267) |
| Electricity for lighting                          | (232) x                   | 0.519 =                              | 144.81 (2                       | 268) |
| Energy saving/generation technologies<br>Item 1   |                           | 0.519 =                              | -386.8                          | 269) |
| Total CO2, kg/year                                |                           | sum of (265)(271) =                  | 714.86 (2                       | 272) |
| CO2 emissions per m²                              |                           | (272) ÷ (4) =                        | 11.59 (2                        | 273) |
| El rating (section 14)                            |                           |                                      | 91 (2                           | 274) |
| 13a. Primary Energy                               |                           |                                      |                                 |      |
|   | <b>Energy</b><br>kWh/year | <b>Primary</b><br>factor             | <b>P. Energy</b><br>kWh/year    |      |
| Space heating (main system 1)                     | (211) x                   | 1.22 =                               | 2689.14 (2                      | 261) |
| Space heating (secondary)                         | (215) x                   | 3.07 =                               | 0 (2                            | 263) |
| Energy for water heating                          | (219) x                   | 1.22 =                               | 2376.86 (2                      | 264) |
| Space and water heating                           | (261) + (262) + (263)     | + (264) =                            | 5066 (2                         | 265) |
| Electricity for pumps, fans and electric keep-hot | (231) x                   | 3.07 =                               | 354.48 (2                       | 267) |
| Electricity for lighting                          | (232) x                   | 0 =                                  | 856.56 (2                       | 268) |
| Energy saving/generation technologies<br>Item 1   |                           | 3.07 =                               | -2288.02                        | 269) |
| 'Total Primary Energy                             |                           | sum of (265)(271) =                  | 3989.03 (2                      | 272) |
| Primary energy kWh/m²/year                        |                           | (272) ÷ (4) =                        | 64.65 (2                        | 273) |

# SAP 2012 Overheating Assessment



Calculated by Stroma FSAP 2012 program, produced and printed on 25 March 2019

## Property Details: 01-19-73120 A-1-05 PL1

| Dwelling type:<br>Located in:<br>Region:<br>Cross ventilation possible:<br>Number of storeys:<br>Front of dwelling faces:<br>Overshading:<br>Overhangs:<br>Thermal mass parameter:<br>Night ventilation:<br>Blinds, curtains, shutters:<br>Ventilation rate during hot weat<br>Overheating Details: | her (ach):   | Flat<br>England<br>Thames valley<br>No<br>1<br>North East<br>Average or unknown<br>None<br>Calculated 103.32<br>False<br>4 ( Windows fully ope | en)  |  |
|---|--|--|--|--|
| Summer ventilation heat loss co<br>Transmission heat loss coeffici  |  | 208.5<br>48.6  |  | (P1)   |
| Summer heat loss coefficient:   |  | 257.09   |  | (P2)   |
| Overhangs:  |  |  |  |  |
| Orientation:Ratio:South West (Rear Elev)0South West (Rear Elev Balconny)North West (Side Elev)0   | <b>Z_overhangs:</b><br>1<br>0.53<br>1  |  |  |  |
| Solar shading:  |  |  |  |  |
|   |  |  |  |  |
| Orientation:Z blindsSouth West (Rear Elev)1South West (Rear Elev Balcony)North West (Side Elev)1Solar gains:  | : Solar access:<br>0.9<br>0.9<br>0.9<br>0.9  | Overhangs:<br>1<br>0.53<br>1   | <b>Z summer:</b><br>0.9<br>0.43<br>0.9                     | (P8)<br>(P8)<br>(P8)                               |
| South West (Rear Elev) 1<br>South West (Rear Elev Balcony)<br>North West (Side Elev) 1<br>Solar gains:<br>Orientation<br>South West (Rear Elev) 0.9 x<br>South West (Rear Elev Balconxy)  | 0.9<br>0.9   | 1<br>0.53  | 0.9<br>0.43  | (P8)   |
| South West (Rear Elev) 1<br>South West (Rear Elev Balcony)<br>North West (Side Elev) 1<br>Solar gains:<br>Orientation<br>South West (Rear Elev) 0.9 x<br>South West (Rear Elev Balconxy)  | 0.9<br>0.9<br>0.9<br>Area Flux<br>8.1 119.92<br>6.41 119.92  | 1<br>0.53<br>1<br><b>g_ FF</b><br>0.4 0.8<br>0.4 0.8   | 0.9<br>0.43<br>0.9<br><b>Shading</b><br>0.9<br>0.43<br>0.9 | (P8)<br>(P8)<br>Gains<br>251.78<br>95.48<br>156.29 |
| South West (Rear Elev) 1<br>South West (Rear Elev Balcony)<br>North West (Side Elev) 1<br>Solar gains:<br>Orientation<br>South West (Rear Elev) 0.9 x<br>South West (Rear Elev Balconxy)<br>North West (Side Elev) 0.9 x  | 0.9<br>0.9<br>0.9<br><b>Area Flux</b><br>8.1 119.92<br>6.41 119.92<br>6.1 98.85<br>re (Thames valley)<br>hent<br><b>berature</b> | 1<br>0.53<br>1<br><b>g_</b><br>0.4<br>0.4<br>0.4<br>0.8<br>0.8<br>0.8<br>0.8<br>0.8<br>0.8<br>0.8<br>0.8                                       | 0.9<br>0.43<br>0.9<br><b>Shading</b><br>0.9<br>0.43<br>0.9 | (P8)<br>(P8)<br>Gains<br>251.78<br>95.48<br>156.29 |